

## **Nanosized Natural Minerals as Sustainable Fillers for Near-Infrared Shielding Coatings: Comparative Study of Rutile, Leucosene, Ilmenite, and Hydroilmenite**

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### **Abstract**

This study investigates nanosized Thai natural minerals rutile, leucosene, ilmenite, and hydroilmenite as sustainable fillers for near-infrared (NIR) shielding coatings. The minerals, mainly composed of TiO<sub>2</sub>, were processed by high-energy ball milling without chemical additives. The resulting natural mineral nanopowders were subsequently dispersed into a polyvinyl alcohol (PVA) matrix and applied as thin film coatings. The optical and thermal performance was found to be highly dependent on the resulting particle size and elemental composition. Specifically, the TiO<sub>2</sub>-rich rutile and leucosene coatings primarily enhanced IR reflection, whereas the iron-rich ilmenite and hydroilmenite coatings significantly improved NIR absorption. Critically, the ilmenite coating achieved optimal thermal performance, resulting in a maximum reduction of the model house interior temperature by 3 °C compared to the unmodified PVA film. These findings confirm the feasibility of utilizing locally sourced, processed natural minerals as cost-effective and environmentally friendly alternatives to synthetic nanomaterials, demonstrating a promising pathway for developing high-performance, energy-saving coatings.

**Keywords:** Near-infrared (NIR) shielding, Natural minerals, Sustainable coatings, High-energy ball milling, Nanoparticles, Thermal performance

### **1. Introduction**

Rising global temperatures and rapid urbanization have intensified heat accumulation in buildings, leading to increased cooling energy demand, accelerated photochemical smog formation, and heightened risks to public health. Surface overheating is primarily driven by near-infrared (NIR) solar radiation, which accounts for more than half of the total heat load absorbed by building envelopes [1]-[2]. Consequently, advanced infrared (IR)-shielding materials have emerged as essential components in passive cooling technologies aimed at reducing indoor temperatures and alleviating the energy burden associated with air-conditioning systems. A wide range of IR/NIR shielding materials, including metals, transparent conductive oxides (TCOs), plasmonic NIR absorbers (e.g., CuS, Cu<sub>2-x</sub>S) [3], polymer-based IR absorbers [4], and 2D nanomaterials, including graphene derivatives, have been developed to modulate solar heat gain [5]-[7]. However, many of these require complex synthesis, expensive precursors, or toxic solvents, limiting their scalability and sustainability. Among them, a widely studied material for optical and thermal management, titanium dioxide (TiO<sub>2</sub>) has gained particular attention owing to its abundance, high refractive index, photostability, chemical stability, cost-efficiency, and strong light-matter interactions efficient UV and NIR responses. Its anatase and rutile polymorphs have been widely employed in coatings, smart windows, and photocatalysts, and optical coatings for thermal-management systems [8]-[11]. The optical and thermal-shielding properties of TiO<sub>2</sub>-based materials are known to vary considerably with crystal phase, dopant concentration, and microstructural design. Anatase TiO<sub>2</sub> generally provides high NIR reflectance due to its wide band gap

and relatively low absorption coefficient, whereas rutile and doped TiO<sub>2</sub> phases, particularly those enriched with transition metals such as Fe, are more effective NIR absorbers, owing to enhanced free-electron densities and localized electronic transitions. The introduction of F<sup>-</sup> ions or Fe<sup>3+</sup> dopants can generate Ti<sup>3+</sup> species and oxygen vacancies, which facilitate localized surface plasmon resonance (LSPR) in the NIR region, thereby improving absorption efficiency [12]-[13]. Moreover, core-shell and yolk-shell nanostructures, such as Fe<sub>2</sub>O<sub>3</sub>@SiO<sub>2</sub>@TiO<sub>2</sub> composites, have demonstrated superior NIR shielding due to their multi-phase interfaces, refractive index mismatch, and controllable light-scattering pathways. Notably, nanocomposites incorporating amorphous Fe<sub>2</sub>O<sub>3</sub> coated with TiO<sub>2</sub> and spaced by SiO<sub>2</sub> interlayers exhibit improved NIR reflectance [14]. Similarly, TiO<sub>2</sub>/(Fe,Mn)<sub>2</sub>O<sub>3</sub> composite pigments prepared by spray pyrolysis show a significant linear increase in NIR reflectance with rising TiO<sub>2</sub> content, attributed to interfacial scattering, optical dilution, and phase-contrast effects. The optimized composite exhibited a total NIR reflectance of 21.0%, representing a 41% enhancement over pure (Fe,Mn)<sub>2</sub>O<sub>3</sub>, and reduced surface temperature by 6.9 °C under IR exposure [15]. These findings underscore the importance of phase composition, particle morphology, and nanostructural engineering in designing energy-saving coatings. Of particular interest to the present study is that several of these high-performance composite architectures, such as Fe<sub>2</sub>O<sub>3</sub>@TiO<sub>2</sub> and Fe<sub>2</sub>O<sub>3</sub>@SiO<sub>2</sub>@TiO<sub>2</sub> are synergistic thermal shielding effect mechanism [16]. Therefore, Fe-Ti-Si oxide phases occur naturally in leucoxene and hydroilmenite, suggesting that thermally functional optical properties can be harnessed from low-cost, earth-abundant mineral sources without extensive chemical modification.

Nevertheless, most IR-shielding studies focus on purified or synthetically modified TiO<sub>2</sub> nanoparticles, which involve energy-intensive and chemically hazardous processes. In contrast, natural titanium minerals such as rutile, leucoxene, ilmenite, and hydroilmenite serve as major industrial raw materials for TiO<sub>2</sub> production and are available in large quantities at low cost [17]-[20]. These minerals contain intrinsic mixtures of TiO<sub>2</sub> and iron oxides and small impurities. These multiphase compositions can simultaneously enable IR reflectance and absorption, offering unique optical and electronic features over purified TiO<sub>2</sub>. Despite their abundance and economic advantages, their direct use in functional thermal-shielding coatings remains largely unexplored. Most existing studies have focused on high-purity TiO<sub>2</sub> grades or modified Ti-based composites, which significantly increases material cost and limits large-scale implementation. Using natural minerals directly without chemical purification or a complex modification process offers a sustainable and economically attractive alternative for IR-shielding coatings. When reduced to the nanoscale, these minerals can exhibit enhanced dispersion, increased surface area, and modified optical interactions, all of which are beneficial for NIR attenuation. Despite these advantages, there is currently a lack of comparative, nanoscale studies assessing the IR-shielding behavior of different Ti-bearing natural minerals. Moreover, the structure-property relationships that govern their effectiveness as functional fillers in polymer-based NIR-shielding coatings remain poorly understood. High-energy ball milling (HEBM) is a well-established method for mineral refinement and can efficiently reduce particle size while preserving the intrinsic mineralogical features, a mechanochemical technique known to induce crystallographic disorder, reduce particle dimensions, and improve interfacial adhesion within composites. Our previous studies have demonstrated the efficacy of acid-assisted ball milling in activating ilmenite by modifying its surface characteristics, thereby improving its suitability for subsequent composite formation. Likewise, heterojunction nanocomposites synthesized from milled ilmenite and leucoxene have shown enhanced electrochemical performance due to increased surface area and favorable phase interactions [21]-[22]. To enhance the dispersion, surface activity, and particle size uniformity of the mineral ore fillers, this work therefore employs HEBM. However, the application of this technique across a broader set of Ti-rich natural minerals has not been comprehensively explored in the context of optical thermal shielding. Moreover, no prior study has simultaneously evaluated the IR-shielding performance of nanosized rutile, leucoxene, ilmenite, and hydroilmenite processed via identical milling conditions when incorporated into a polyvinyl alcohol (PVA) matrix. The mineralogical diversity among rutile, leucoxene, ilmenite, and hydroilmenite, particularly variations in TiO<sub>2</sub> content, Fe-oxide phases, defects, and nanostructures, influence on milling condition may strongly influence their suitability as NIR-shielding fillers. We hypothesize that the optical and thermal-shielding behaviors of nanosized natural minerals are governed by their intrinsic mineral composition and nanoscale structural features.

Specifically, minerals with higher TiO<sub>2</sub> content and optimized Fe-oxide components (e.g., rutile and leucoxene) are expected to show a different effect on NIR attenuation relative to ilmenite and hydroilmenite. This study investigates the NIR-shielding efficiency of nanosized Thai natural minerals rutile, leucoxene, ilmenite, and hydroilmenite incorporated into polyvinyl alcohol (PVA) coatings. By correlating their mineralogical characteristics with optical transmission and thermal-management performance, we aim to clarify the structure–property relationships governing their effectiveness as sustainable, low-cost fillers for energy-saving coatings. This work provides the first comparative analysis of these minerals at the nanoscale, highlighting their potential as locally sourced functional materials for passive cooling and building-energy-efficiency applications.

PVA is selected as the polymeric matrix in this study for its excellent film-forming ability, non-toxicity, optical clarity, and compatibility with inorganic fillers. PVA-based coatings have demonstrated high mechanical flexibility, tunable thermal stability, and ease of processing in water-based systems, which are suitable for environmentally friendly surface coatings. Furthermore, PVA supports homogeneous dispersion of nanostructured additives without the use of harmful organic solvents and can be engineered into multifunctional membranes with improved durability when combined with appropriate reinforcements [23]. Nonetheless, although the inherent hydrophilicity of PVA presents limitations for outdoor deployment, particularly under humid or rain-exposed conditions, its favorable film-forming ability, solution processability, and compatibility with a wide range of particulate fillers make it an ideal model polymer for initial investigations. In this context, PVA serves as a practical and accessible platform for evaluating the near-infrared (NIR) shielding efficacy of mineral-based nanofillers. Furthermore, its surface properties can be readily modified through hydrophobic coating techniques or chemical crosslinking, thereby improving moisture resistance. In future applications, insights gained from PVA-based composites may inform the design of more robust and durable coatings employing alternative, weather-resistant polymer matrices. Additionally, PVA-based films may still be effectively employed as interior or interlayer coatings, particularly in thermal shielding applications where direct exposure to moisture is limited [24]-[25].

## 2. Experimental

### 2.1 Materials

Natural minerals rutile, leucoxene, ilmenite, and hydroilmenite were obtained from local sources in Thailand (Sakorn Minerals Co., Ltd., Prachuap Khiri Khan Province, southern Thailand). Polyvinyl alcohol (PVA, analytical grade) was purchased from Chem-supply. All chemicals were used as received without further purification. Deionized water was used in all preparations.

**Table 1.** Names of the experimental conditions at constant milling time.

Natural mineral- based	400 rpm	500 rpm	600 rpm
Rutile	Ru 400 rpm	Ru 500 rpm	Ru 600 rpm
Leucoxene	Le 400 rpm	Le 500 rpm	Le 600 rpm
Ilmenite	Il 400 rpm	Il 500 rpm	Il 600 rpm
Hydroilmenite	Hy 400 rpm	Hy 500 rpm	Hy 600 rpm

**Table 2.** Names of the experimental conditions at constant milling speed.

Natural mineral- based	30 minutes	60 minutes	90 minutes	120 minutes
Rutile	Ru 30 min	Ru 60 min	Ru 90 min	Ru 120 min
Leucoxene	Le 30 min	Le 60 min	Le 90 min	Le 120 min
Ilmenite	Il 30 min	Il 60 min	Il 90 min	Il 120 min
Hydroilmenite	Hy 30 min	Hy 60 min	Hy 90 min	Hy 120 min

## 2.2 Preparation of TiO<sub>2</sub>-Based Powders from Natural Minerals

The natural minerals (rutile, leucosene, ilmenite, and hydroilmenite) were mechanically milled using a high-energy planetary ball mill (model: Planet M2-3F, Nagao System) equipped with zirconia milling jars and zirconia balls (3 mm diameter). The ball-to-powder mass ratio was fixed at 10:1, and no chemical additives were used during the process.

The milling procedure was carried out in two stages: Stage 1: Effect of Milling Speed: To identify the optimal rotational speed, milling was performed at 400, 500, and 600 revolutions per minute (rpm) for a fixed duration of 60 min. The extent of comminution was evaluated by comparing the particle size distributions of the milled powders. Samples were designated according to the conditions used (Table 1). Stage 2 Effect of Milling Time: Based on the results of Stage 1, the speed that yielded the smallest average particle size was selected for subsequent experiments. At this optimized speed, milling time was systematically varied at 30, 60, 90, and 120 minutes to investigate the influence of grinding duration on particle size reduction and crystallinity. The corresponding samples were designated as summarized in Table 2. After milling, all powders were collected, dried at room temperature, and stored in airtight containers to prevent contamination and moisture uptake before further characterization and coating preparation.

## 2.3 Characterization

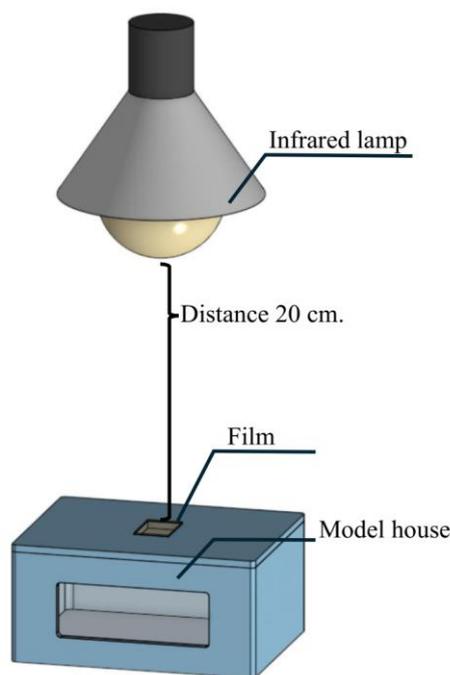
The chemical compositions of the mineral samples were analyzed by X-ray fluorescence (XRF; Rigaku, ZSX PrimusI) for chemical composition determination. Crystal structures were examined by X-ray diffraction (XRD; SmartLab, Rigaku) employing Cu K $\alpha$  radiation ( $\lambda = 1.5406 \text{ \AA}$ ), and the average crystallite sizes were estimated using the Scherrer equation. Particle morphology was observed by scanning electron microscopy (SEM; S-8030, HITACHI). Optical transmittance and reflectance spectra across the 240–2600 nm wavelength range were measured using a UV–vis–NIR spectrophotometer (UH4150, HITACHI).

## 2.4 Preparation of Mineral–PVA Thin-Film Coatings

For coating preparation, a 10 wt% PVA solution was prepared by dissolving PVA in deionized water at 90 °C under continuous magnetic stirring until complete dissolution was achieved. This concentration was selected due to its optimal viscosity for film formation via the doctor-blade technique. The 10 wt% solution facilitates uniform spreading, offers adequate binding strength to prevent particle detachment, and is commonly employed as a standard formulation for comparative thermal shielding studies. After stirring for 2 h, homogeneity was confirmed by visual inspection of the suspension in a transparent container. The absence of undissolved particulates or sedimentation at the bottom of the vessel indicated complete dispersion of the PVA polymer. At this point, the milled mineral powders were added to the solution at a loading of 0.5 wt%. To aid dispersion, 0.5 wt% sodium dodecylsulfate (SDS) surfactant was added, and the suspension was stirred for an additional 10 min, subsequent loading under ultrasonicated irradiation to ensure homogeneous mixing. The resulting mixture was blade-coated onto glass substrates ( $2.5 \times 3.75 \text{ cm}^2$ ) using a doctor blade with a 0.03 mm gap, a speed of  $5 \text{ mm s}^{-1}$ , and a coating length of 150 mm, and dried at room temperature.

## 2.5 Thermal Performance Test

The thermal shielding performance of the mineral–PVA composite films was assessed using custom-fabricated model house structures (external dimensions: 100 mm height  $\times$  135 mm width  $\times$  175 mm length; wall thickness: 10 mm), yielding an internal volume of approximately 1856.25 cm<sup>3</sup>. The structures were fabricated from heat-resistant PETG plastic. Coated glass slides on which the mineral–PVA films were deposited were placed at the top opening of each model house to simulate incident sunlight entering through a window. All samples' assembled structures were exposed to simulated solar radiation (Philips Infrared BR125 250w E27, 1000 lux) under controlled conditions illustrated in Fig. 1. Internal air temperatures were recorded at fixed time intervals using calibrated digital thermometers (DHT22 AM2302 temperature and humidity sensor module), and results were compared against uncoated control structures to evaluate the relative thermal shielding efficacy of each film formulation.



**Fig. 1.** Schematic illustration of the custom-fabricated model house used to evaluate the thermal shielding performance of mineral–PVA composite films.

### 3. Result and Discussion

#### 3.1 Chemical Composition of Natural Minerals

Chemical composition analysis of the four natural minerals rutile, leucoxene, ilmenite, and hydroilmenite was summarized in Table 3, where titanium dioxide ( $\text{TiO}_2$ ) was identified as the primary constituent, with mass percentages of 91.82%, 87.60%, 58.80%, and 67.93%, respectively. Secondary phase components for silicon dioxide ( $\text{SiO}_2$ ) were presented in rutile (3.69%) and leucoxene (7.02%), while iron (III) oxide ( $\text{Fe}_2\text{O}_3$ ) was found in ilmenite (26.34%) and hydroilmenite (21.99%). These secondary constituents are likely to affect material properties such as infrared reflectance and heat absorption, which are key factors for potential applications in thermal-protective coatings [1]-[2].

**Table 3.** Chemical composition of natural mineral-based samples.

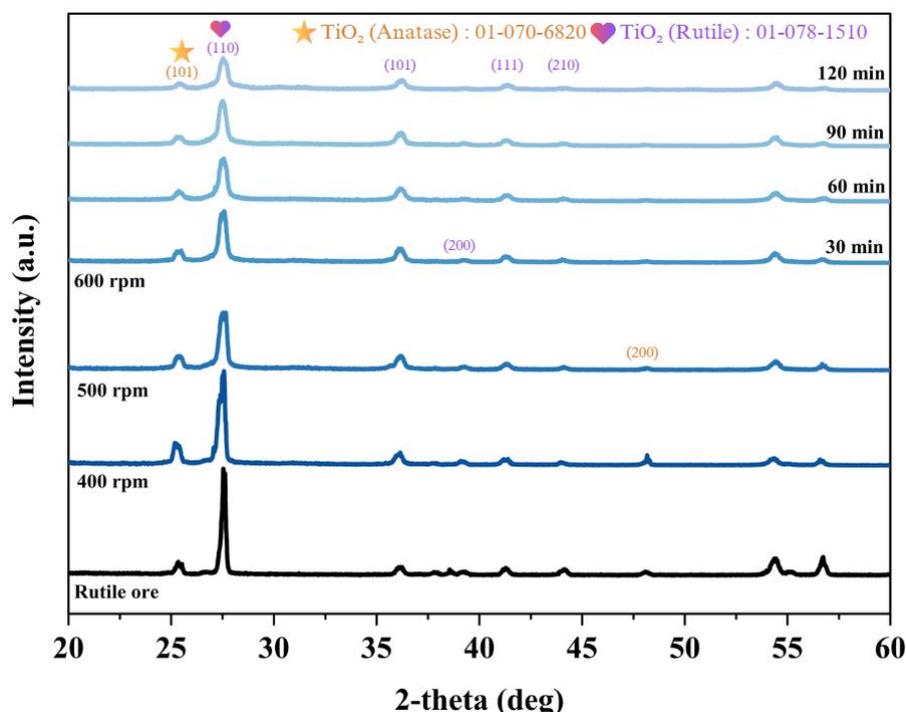
Chemical Composition Weight %	$\text{TiO}_2$	$\text{Fe}_2\text{O}_3$	$\text{SiO}_2$	$\text{Al}_2\text{O}_3$	$\text{Cr}_2\text{O}_3$	$\text{ZrO}_2$	$\text{K}_2\text{O}$	$\text{MnO}$
Rutile	91.82	0.70	3.69	1.04	0.1	1.69	0.16	-
Leucoxene	87.60	0.92	7.02	1.80	0.33	1.15	0.28	-
Ilmenite	58.80	26.34	3.02	3.76	0.79	1.56	0.02	0.97
Hydroilmenite	67.93	21.99	1.93	1.61	1.49	0.71	0.04	0.71

#### 3.2 Crystal Structure of Natural Minerals and Nanostructured Minerals

Figure 2 presents the X-ray diffraction (XRD) patterns of rutile mineral before and after high-energy mechanical milling at various conditions. Both the as-received rutile and all the samples milled at 400–600 rpm for 60 min, as well as at a constant speed of 600 rpm for 30–120 min, exhibit diffraction peaks corresponding to the main phase of rutile  $\text{TiO}_2$  [JCPDS 01-078-1510], with reflections at  $27.51^\circ$ ,  $36.16^\circ$ ,  $39.29^\circ$ ,  $41.33^\circ$ ,  $44.16^\circ$ ,  $54.46^\circ$ , and  $56.78^\circ$  assigned to the (110), (101), (200), (111), and (210), planes, respectively. Weak anatase-phase signals [JCPDS 01-070-6820] at  $25.42^\circ$  and  $48.23^\circ$  are also observed under certain conditions. No additional peaks attributable to impurity phases are detected.

Although XRF results show in Table 3 indicate that the rutile contains approximately 3.69 wt% SiO<sub>2</sub> before and after milling, the low concentration and poor crystallinity (likely amorphous) of SiO<sub>2</sub> explain the absence of distinct SiO<sub>2</sub> peaks in the XRD patterns [26]. A progressive decrease in the peak intensities with increasing milling speed and duration indicates a reduction in the crystallinity of TiO<sub>2</sub>. Crystallite sizes, calculated using the Scherrer equation and summarized in Table 4, show that the initial crystallite size of as-received rutile is 40.2 nm, which is larger than that of the milled samples at 600 rpm. This observation can be attributed to the geological formation of natural rutile under prolonged high temperature and pressure, which promotes a highly ordered crystal structure [27]. With increasing milling speed and time, the crystallite size decreases to 30.87, 24.47, 22.04, and 19.51 nm at 600 rpm for 30, 60, 90, and 120 min, respectively. At lower speeds, shear forces dominate over impact forces, causing only minor disruption of the crystal lattice. This reduction in crystallite size correlates with the observed decrease in particle size [28]-[30].

The natural leucosene and high-energy mechanically milled leucosene revealed that corresponding to TiO<sub>2</sub> in the rutile phase structure with a secondary phase structure of anatase (Fig. 3). In addition, an  $\alpha$ -SiO<sub>2</sub> peak [JCPDS 01-077-1060] was detected at 26.68° on the (011) plane in the unmilled leucosene, attributable to its 7.02 % SiO<sub>2</sub> content, which renders the  $\alpha$ -SiO<sub>2</sub> peak more distinct than in rutile. However, this  $\alpha$ -SiO<sub>2</sub> peak disappeared after milling due to particle and crystallite size reduction, contribute with TiO<sub>2</sub> peak overlap and masking [29]. No extraneous phases were observed overall, but the TiO<sub>2</sub> peak intensities progressively decreased with increasing milling speed, indicating reduced crystallinity and crystallite size. The average crystallite size of TiO<sub>2</sub> (rutile) on the (110) plane decreased markedly from 76.55 nm in the pristine sample to 19.86 nm at the highest milling speed. Furthermore, Table 4 shows that at 600 rpm for 30–120 min, the average crystallite size decreased from 24.48 nm at 30 min to 14.24 nm at 60 min [31] before increasing to 14.63 nm and 17.66 nm at 90 and 120 min, respectively, likely due to the aggregation of small crystallites via mechanochemical reactions [28], [32]. Moreover, leucosene contained a high proportion of TiO<sub>2</sub> in the rutile phase, which remains highly stable when the crystallite size exceeds ~14 nm. When sufficient energy is supplied, however, TiO<sub>2</sub> can transform into other phases because the surface energy of rutile is substantially higher than that of anatase [33]. Notably, when the crystallite size approached ~14 nm, slight instability of rutile occurred, promoting phase transformation or coalescence into anatase [27].



**Fig. 2.** X-ray diffraction patterns of rutile minerals milled at different rotational speeds and durations.

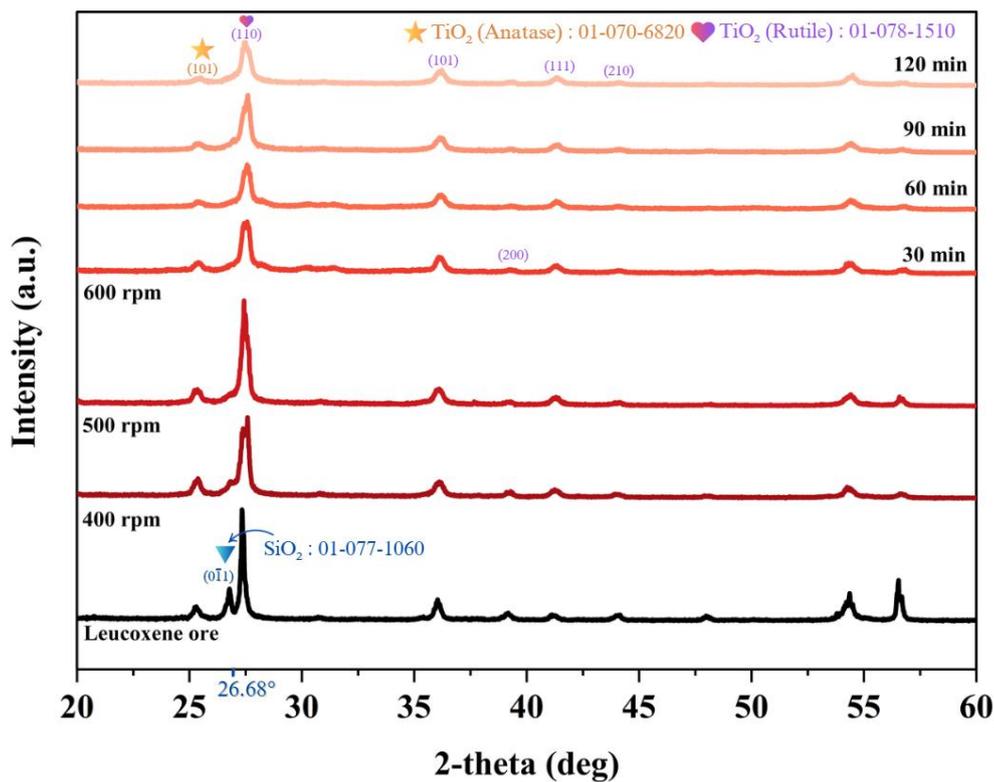


Fig. 3. X-ray diffraction patterns of leucoxene minerals milled at different rotational speeds and durations.

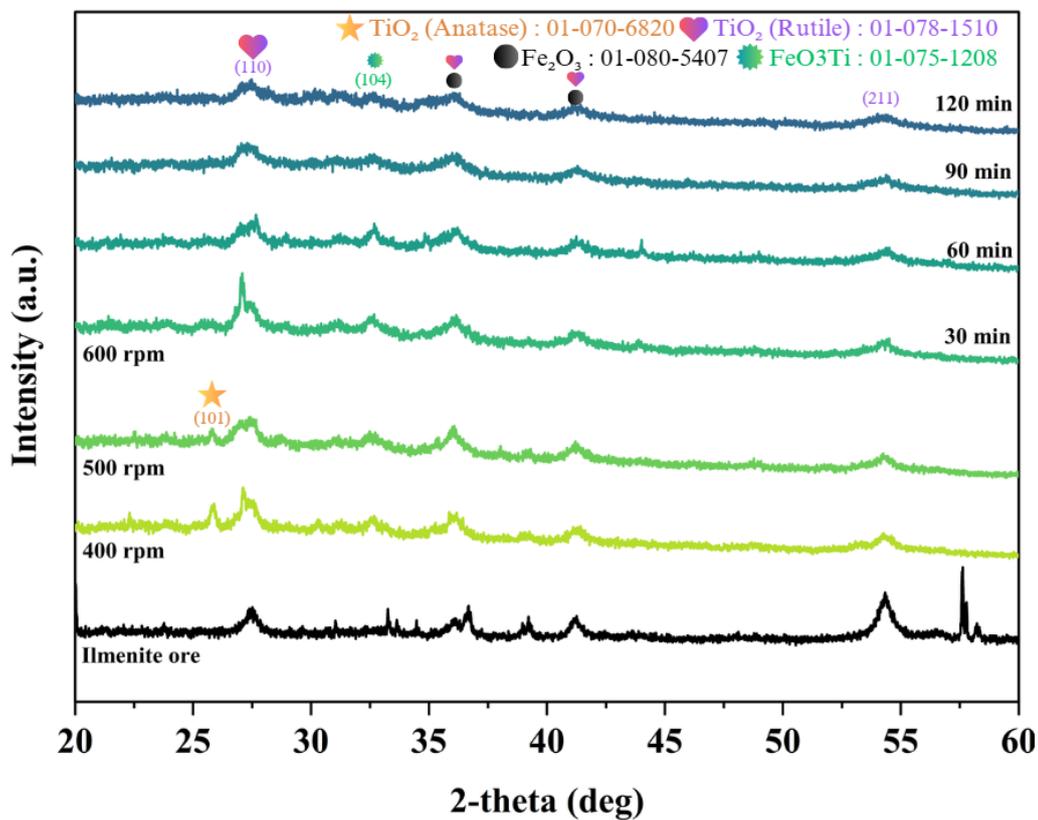


Fig. 4. X-ray diffraction patterns of ilmenite minerals milled at different rotational speeds and durations.

The natural ilmenite and mechanically milled ilmenite (Fig. 4) revealed that all unmilled and milled samples exhibited diffraction patterns consistent with  $\text{TiO}_2$  in the rutile phase with main peaks at  $27.49^\circ$ ,  $36.03^\circ$ ,  $41.22^\circ$ , and  $54.35^\circ$  corresponding to the (110), (101), (111), and (211) planes, respectively. Additional peaks corresponding to  $\text{Fe}_2\text{O}_3$  [JCPDS 01-080-5407] at  $36.03^\circ$  and  $41.22^\circ$  in the (110) and (113) planes overlapped with  $\text{TiO}_2$  (rutile) peaks, along with  $\text{FeTiO}_3$  [JCPDS 01-075-1208] at  $32.51^\circ$  in the (104) plane, indicating the coexistence of these phases. Milling also induced the appearance of anatase  $\text{TiO}_2$  at  $25.31^\circ$ . Overall, the peak intensities varied with increasing rotation speed, reflecting crystallite size changes due to mechanochemical reactions and fragmentation from high kinetic energy, where increased shear and impact forces led to a reduction in crystallite size at higher rotation speeds [29]. As shown in Table 4, the minimum average crystallite size of 5.28 nm was obtained at 600 rpm, demonstrating the trend of decreasing particle and crystallite sizes of ilmenite prepared by high-energy mechanical milling with increasing milling duration.

The hydroilmenite minerals shown in Fig. 5 exhibited diffraction patterns consistent with the rutile  $\text{TiO}_2$  and  $\text{Fe}_2\text{O}_3$  phase in addition to anatase  $\text{TiO}_2$ , corresponding to the high  $\text{TiO}_2$  content in hydroilmenite (67.93%) as determined by XRF. The crystal size also decreased significantly with increasing rotational speed, and when continuously grinding at a constant speed of 600 rpm for 30–120 min, the average crystal size slightly increased from 5.80 to 5.90 nm after 60–90 min (Table 4), which could be due to the mechanically induced crystallization from the small size of  $\text{TiO}_2$  (rutile) crystals. However, after continuous grinding for 120 min, the average crystal size decreased to a minimum of 4.30 nm, reflecting the trend of decreasing particle size and crystallinity of hydroilmenite with grinding time. [28], [29], [32], [33]. High-energy ball milling successfully reduced the particle size of rutile, leucoxene, ilmenite, and hydroilmenite into the nanometer range without chemical additives. XRD patterns confirmed the preservation of the crystalline phases after milling, with minor broadening of peaks consistent with crystallite sizes decreased. Among the samples, rutile and leucoxene showed higher crystallinity, while ilmenite and hydroilmenite exhibited mixed oxide phases containing Ti and Fe.

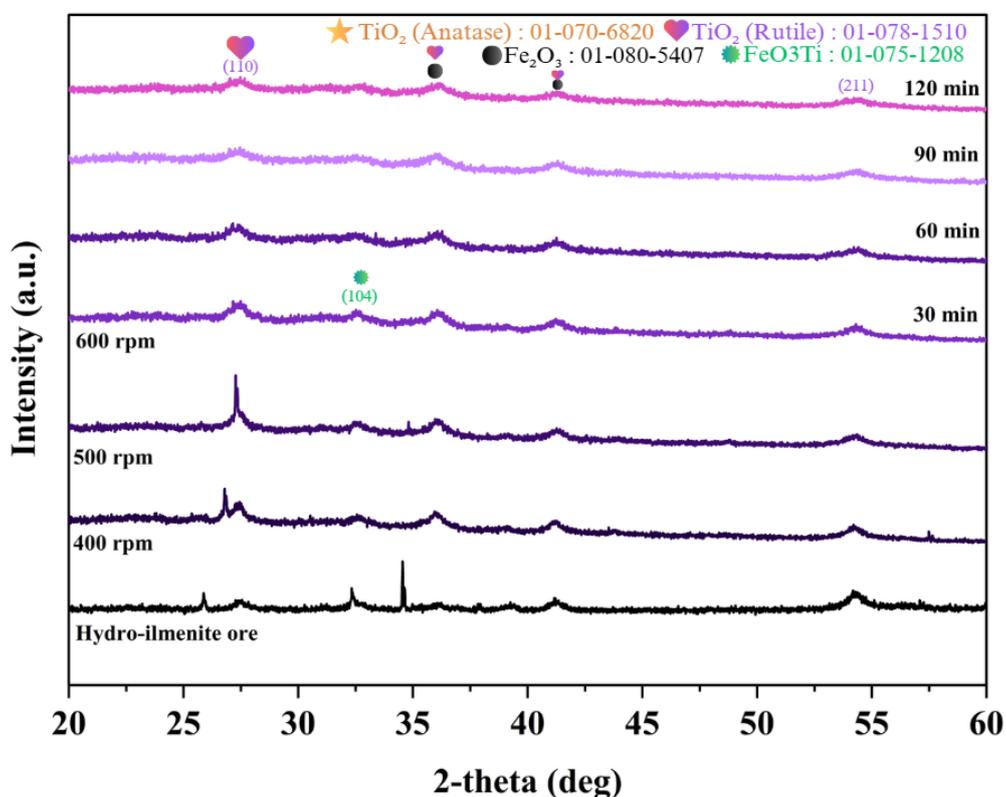
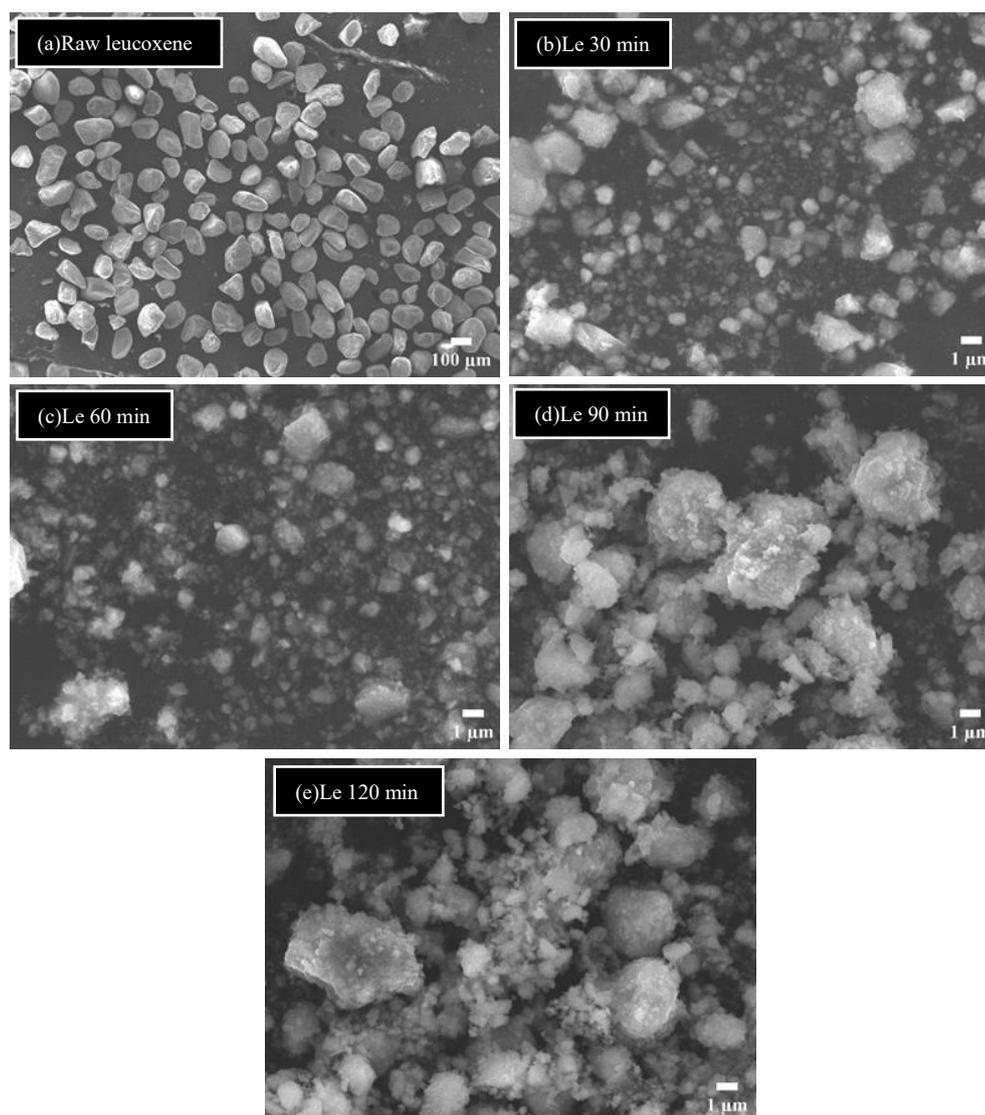


Fig. 5. X-ray diffraction patterns of hydroilmenite minerals milled at different rotational speeds and durations.

**Table 4.** Mean crystallite size of natural mineral-based powders before and after milling at 600 rpm for different durations.

Natural mineral-based	Mean crystal size (nm)				
	Raw mineral	30 minute	60 minute	90 minute	120 minute
Rutile	40.42	24.42	16.81	18.00	14.47
Leucoxene	63.89	24.48	14.24	14.63	17.66
Ilmenite	79.75	21.80	9.17	6.04	5.28
Hydroilmenite	89.65	6.65	5.80	5.90	4.30



**Fig. 6.** SEM images of leucoxene minerals milled at 600 rpm for varying durations: (a) before milling, (b) 30 min, (c) 60 min, (d) 90 min, (e) 120 min.

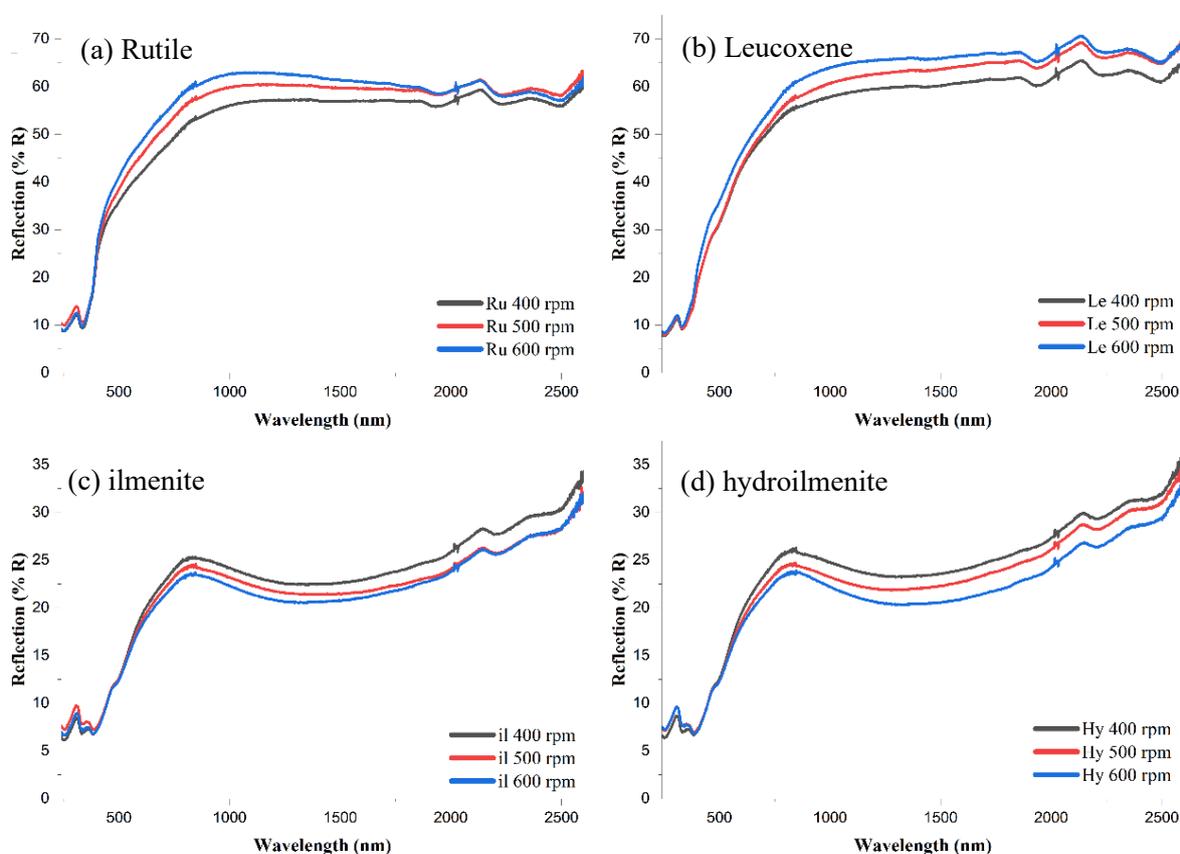
### 3.3 Morphology of Milled Natural Mineral Powders

SEM images (Fig. 6) show that the morphological characteristics of leucoxene before and after high-energy mechanical milling, minerals consist of irregular micron-sized particles with partial agglomeration, which is a typical characteristic of mechanically milled oxide powders. After milling at

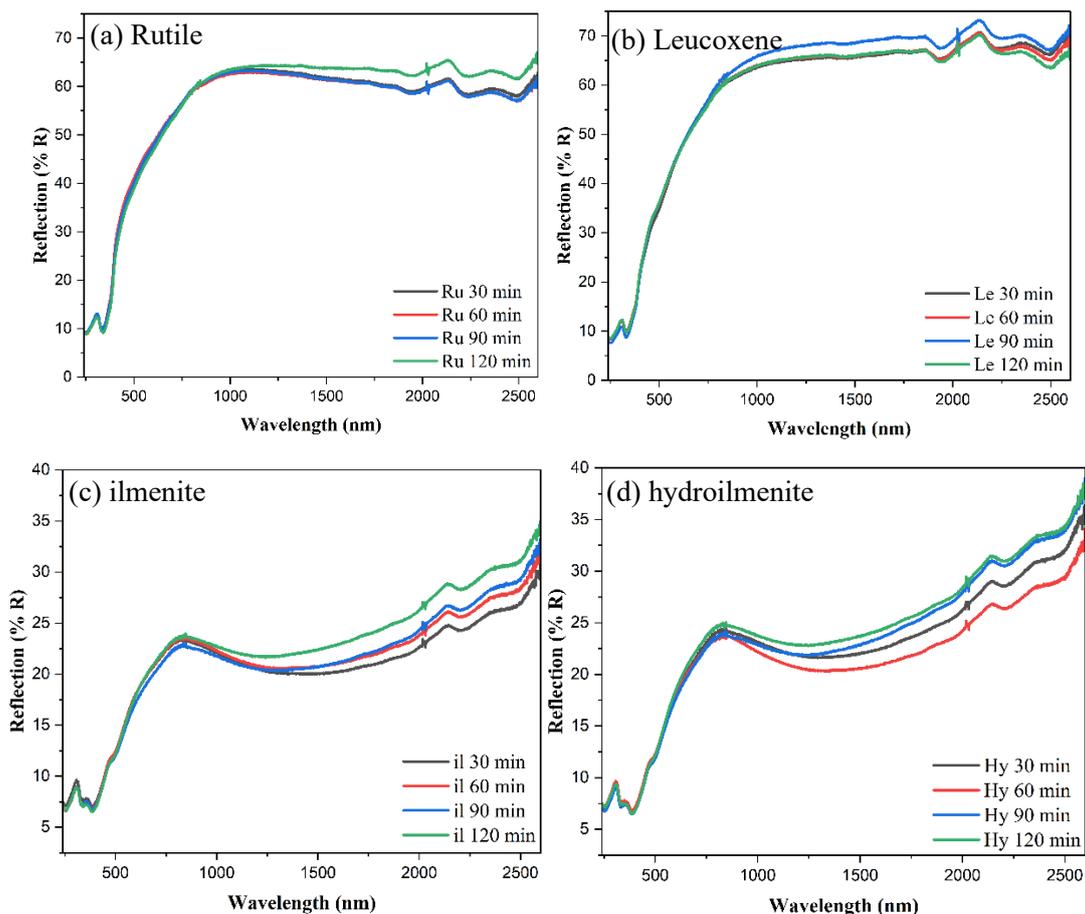
600 rpm (Fig. 6b–e), the powders exhibited more uniform nanosized particles (<100 nm). However, extending the milling time to 90–120 min led to particle agglomeration due to mechanochemical reactions [33], resulting in particle sizes larger than those observed at 30 min. This behavior corresponds to the crystallite size evolution of leucoxene observed by X-ray diffraction analysis. Particle refinement is expected to enhance dispersion in PVA coatings and improve optical interactions.

### 3.4 Optical and NIR Shielding Properties of Natural Mineral

Based on the chemical composition of natural minerals, two subgroups can be distinguished according to their secondary components, which influence thermal radiation shielding properties, such as absorption and reflection. The reflectivity of natural TiO<sub>2</sub>-based minerals, rutile, leucoxene, ilmenite, and hydroilmenite, after high-energy mechanical milling at different rotational speeds of 400, 500, and 600 rpm, is presented in Fig. 7. The reflectivity trends can be classified into two characteristic groups. The first group, comprising (a) rutile and (b) leucoxene, exhibited an increase in reflectivity with increasing rotational speed. Mechanical milling reduced the particle size, producing smaller TiO<sub>2</sub>- and SiO<sub>2</sub>-rich components with a larger surface area, thereby altering their reflectance spectra. Leucoxene demonstrated approximately 4% higher reflectivity in the near-infrared region (800–1500 nm) compared with rutile, attributable to its higher SiO<sub>2</sub> content, which may enhance solar thermal radiation reflectance [2]. The second group, consisting of (c) ilmenite and (d) hydroilmenite, showed a decrease in reflectivity with increasing milling speed, suggesting enhanced absorption properties. This behavior can be explained by their relatively lower TiO<sub>2</sub> and higher Fe<sub>2</sub>O<sub>3</sub> content, with Fe<sub>2</sub>O<sub>3</sub> contributing strongly to solar thermal radiation absorption. Furthermore, both minerals originally exhibited a black, glossy, sandy appearance, but milling reduced particle size and diminished the inherent gloss, increasing surface area and resulting in lower reflectance. These findings suggest that ilmenite and hydroilmenite may serve as effective natural mineral components for coatings designed to enhance solar radiation absorption in heat-protective applications.



**Fig. 7.** UV-Vis-NIR reflectance spectra of mineral powders milled at 400–600 rpm for 60 min: (a) rutile, (b) leucoxene, (c) ilmenite, (d) hydroilmenite.



**Fig. 8.** UV–Vis–NIR reflectance spectra of mineral powders milled at 600 rpm for 30–120 min: (a) rutile, (b) leucoxene, (c) ilmenite, (d) hydroilmenite.

The effect of milling time on reflectance properties of TiO<sub>2</sub>-rich minerals was examined for 30, 60, 90, and 120 minutes (Fig. 8). In the 240–800 nm range (UV to visible light), both rutile and leucoxene minerals exhibited similar reflectance spectra characteristics of their chemical structures and composition. The milled rutile for 120 minutes and leucoxene milled for 90 minutes exhibited the highest reflectance, which may be attributable to the smallest particle size in an optimal range for light scattering, thereby improving reflectance efficiency. The reflectance spectra of ilmenite and hydroilmenite exhibited a continuous increase in near-infrared reflectance with increasing milling time, which can be ascribed to size reduction of the primary TiO<sub>2</sub> and secondary Fe<sub>2</sub>O<sub>3</sub> phases, influencing their optical response. TiO<sub>2</sub> inherently reflects thermal radiation due to its physical properties, while Fe<sub>2</sub>O<sub>3</sub> reflects only partially and strongly absorbs in the lower infrared range owing to its bandgap characteristics. Compared with rutile and leucoxene, ilmenite and hydroilmenite displayed markedly lower reflectance, reflecting their higher absorption capability, particularly due to Fe<sub>2</sub>O<sub>3</sub> content, which effectively absorbs solar thermal radiation. These findings highlight the potential of all four minerals, ilmenite, hydroilmenite, rutile, and leucoxene, as candidate materials for thermal radiation shielding, particularly when incorporated into polymer matrices such as polyvinyl alcohol to develop advanced heat-protective coatings.

The UV–Vis–NIR spectra show distinct optical behaviors depending on mineral type demonstrated that phase composition and structure strongly influence optical properties behavior. Rutile and leucoxene primarily enhanced reflectance in the NIR region (780–2500 nm), consistent with their high TiO<sub>2</sub> content, refractive index and strong light-scattering ability. In contrast, ilmenite and hydroilmenite exhibited stronger NIR absorption due to the presence of Fe<sub>2</sub>O<sub>3</sub>, which acts as an efficient absorber attributed to the Fe<sup>2+</sup>/Fe<sup>3+</sup> ions, which introduce additional electronic transitions. The finer powders (600 rpm) showed enhanced reflection or absorption compared with coarser powders. This

indicates that nanosizing improves optical performance by increasing surface area and light–particle interactions.

### 3.5 Optical Properties of Mineral–PVA Coatings

The optical performance of the mineral–PVA composite coatings was systematically investigated to assess their capability in mitigating heat transfer. Quantitatively assessed by measuring the steady-state interior temperature of a model house apparatus under simulated solar irradiation. To ensure optimal performance for comparison, all mineral samples, rutile, leucosene, ilmenite, and hydroilmenite, were prepared using the smallest particle size milling condition, which was previously determined to provide the highest near-infrared (NIR) reflectance. These milled mineral powders were uniformly dispersed within a PVA matrix and applied as thin film coatings. The results presented in Fig. 9, indicate a notable variation in thermal performance depending on the mineral filler and demonstrate a significant impact of mineral coatings on thermal management. The uncoated control film served as the baseline, recording a maximum steady-state interior temperature of 43.3°C. The application of milled mineral-PVA coatings consistently resulted in a reduction of the interior temperature. The coatings containing rutile, leucosene, ilmenite, and hydroilmenite reduced the temperature to 42.2°C, 42.8°C, 40.3°C, and 42.9°C, respectively. The ilmenite–PVA coating demonstrated the greatest thermal efficacy, achieving a temperature reduction of 3°C compared to the uncoated control. This 3 °C surface temperature reduction represents a significant threshold for practical energy-saving applications in building envelopes. Extensive literature has established quantitative relationships between surface temperature reductions and HVAC energy consumption, demonstrating that a 1 °C decrease in surface temperature corresponds to an 8–12% reduction in HVAC energy consumption, while a 2 °C decrease may yield savings of 15–25% depending on climate and building type [34]–[35]. Thus, the 3 °C reduction observed for ilmenite–PVA coatings translates to a potential energy savings of 20–40% depending on specific building configurations and environmental conditions. These minerals, rich in Fe<sub>2</sub>O<sub>3</sub> content, exhibit strong NIR absorption activity, which directly reduces the amount of heat transmitted through the film. Spectroscopic analysis (Fig. 8) provides insight into the underlying optical mechanisms. Among the mineral fillers, ilmenite and hydroilmenite exhibited the strongest NIR absorption across the 800–2500 nm range, attributable to their high Fe<sub>2</sub>O<sub>3</sub> contents (>45 wt%). By contrast, rutile with negligible Fe content (~2 wt%) displayed minimal absorption. Leucosene, with intermediate iron content, showed moderate absorption. These results suggest a direct correlation between Fe<sub>2</sub>O<sub>3</sub> concentration and NIR absorbance under controlled dispersion conditions. The enhanced absorption can be attributed to the presence of Fe<sup>3+</sup> ions in the hematite ( $\alpha$ -Fe<sub>2</sub>O<sub>3</sub>) phase, which promote d–d electronic transitions and strong ligand field effects. Furthermore, Fe<sub>2</sub>O<sub>3</sub>–TiO<sub>2</sub> interfacial interactions are known to increase free carrier generation, facilitating plasmonic absorption within the NIR region, contributing to broadband absorption and partial reflection in the NIR range, and the TiO<sub>2</sub> phase exhibited NIR reflectivity. Such mechanisms are supported by several studies: Lee, Jung [14] demonstrated that nanostructured Fe<sub>2</sub>O<sub>3</sub>/TiO<sub>2</sub> composites enhanced NIR reflectance via interfacial energy modulation. Similarly, Sadeghi-Niaraki, Ghasemi [16] reported that reddish-brown Fe<sub>2</sub>O<sub>3</sub>@SiO<sub>2</sub>@TiO<sub>2</sub> core–shell nanostructures maintained both visible coloration and high NIR reflectance. Furthermore, Hwang and Jung [15] confirmed that TiO<sub>2</sub>/(Fe,Mn)<sub>2</sub>O<sub>3</sub> composites display enhanced NIR reflectance attributable to synergistic absorption–scattering effects from multivalent iron oxides embedded in a dielectric matrix. While certain core–shell or composite configurations favor NIR reflection, the literature consistently affirms that Fe<sub>2</sub>O<sub>3</sub> contributes substantially to NIR shielding via absorption-dominated mechanisms and/or through enhanced reflectance, depending on its phase structure, dispersion state, and composite architecture. In the present study, an absorption-dominant behavior is most plausible, considering the high Fe<sub>2</sub>O<sub>3</sub> content and the intrinsically dark coloration of the ilmenite-based minerals. These findings underscore the potential of Fe<sub>2</sub>O<sub>3</sub>-rich minerals as viable and sustainable constituents in the design of passive NIR-shielding coatings. Conversely, TiO<sub>2</sub>-rich minerals such as rutile and leucosene are expected to rely primarily on IR/NIR reflection as their principal shielding mechanism. This interpretation is substantiated by experimental and theoretical observations. Spectroscopic data show that rutile- and leucosene-based coatings exhibited the lowest NIR absorbance among all samples (Fig. 8), despite maintaining moderate surface temperature reduction in thermal performance tests. This indicates that heat mitigation in these samples is governed by optical reflection rather than absorption. Rutile TiO<sub>2</sub> is well-documented for its high refractive index ( $n \approx 2.6$ –

2.9 in the NIR region) and low extinction coefficient, both of which facilitate efficient broadband reflection and multiple light scattering [36]-[37]. These properties have been exploited in various architectures: for instance, cotton fabrics coated with rutile TiO<sub>2</sub> exhibited increased NIR reflectivity and reduced thermal loading under solar exposure [38]. Similarly, TiO<sub>2</sub>-based radiative cooling films have shown strong solar reflectivity and NIR backscattering, with performance strongly influenced by particle size and phase composition [39]. Theoretical modelling has further confirmed that TiO<sub>2</sub> retains a high refractive index even at nanoscale dimensions, preserving its capacity for broadband NIR scattering [40]. Additionally, multiple scattering from densely packed rutile structure in the submicron regime particles can significantly enhance reflectance, especially within the NIR range [41]. Among all minerals tested, ilmenite appears to strike the most favorable balance between reflectance (contributed by TiO<sub>2</sub> content) and absorption (associated with Fe<sub>2</sub>O<sub>3</sub> content), thereby delivering superior thermal shielding through a dual-mechanism pathway. The diagram presented in Fig. 10 conceptually illustrates the primary optical mechanisms to govern near-infrared (NIR) shielding performance in natural mineral-based coatings. The overall thermal shielding efficiency results from a synergistic interplay of these mechanisms, modulated by the mineral phase composition, particle morphology, and dispersion quality within the PVA matrix.

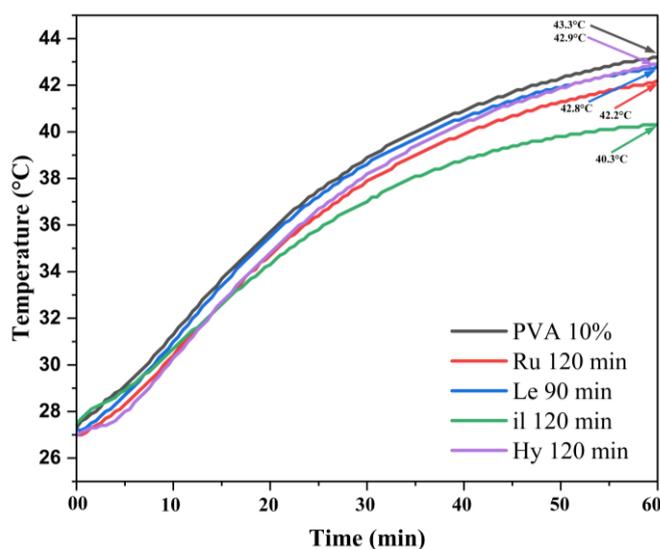


Fig. 9. Internal temperature profiles of model houses coated with PVA films containing rutile, leucoxene, ilmenite, and hydroilmenite.

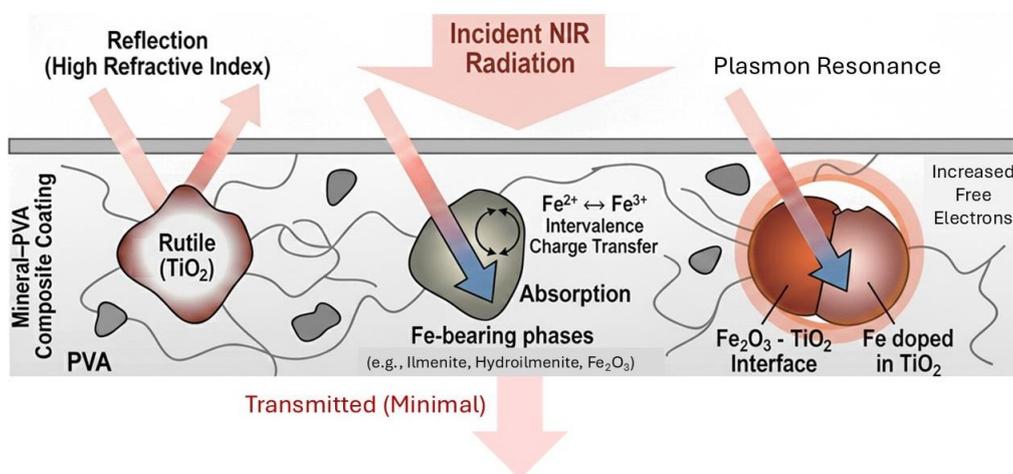


Fig. 10. Schematic illustration of the optical pathways contributing to near-infrared (NIR) shielding in mineral-PVA composite coatings.

## 4. Conclusion

This study successfully investigated the preparation and application of nanosized natural minerals derived from rutile, leucoxene, ilmenite, and hydroilmenite as sustainable functional fillers for near-infrared (NIR) shielding coatings. Utilizing a high-energy mechanical milling (HEMM) process, these minerals were size reduced without the use of chemical reagents and subsequently incorporated into polyvinyl alcohol (PVA) matrices to enhance the infrared (IR) blocking capabilities of the resulting coatings. The comprehensive analysis of milling parameters demonstrated that the milling speed significantly influenced the resultant mineral properties. Milling at 200–600 rpm for a fixed duration (60 minutes) showed that increasing the speed effectively reduced both crystallite and particle sizes. This size reduction directly improved the IR reflectance for the TiO<sub>2</sub>-rich minerals (rutile and leucoxene) and enhanced the heat absorption capacity for the Fe<sub>2</sub>O<sub>3</sub>-containing minerals (ilmenite and hydroilmenite). Further optimization at the superior speed of 600 rpm with varied milling times (30–120 minutes) confirmed continued particle size refinement for rutile, ilmenite, and hydroilmenite. However, leucoxene displayed a tendency toward agglomeration when milled for periods exceeding 60 minutes. The performance evaluation of the final PVA-mineral coatings revealed distinct mechanisms of heat mitigation based on the mineral composition. Rutile and Leucoxene primarily function via a heat reflection mechanism. Ilmenite and Hydroilmenite primarily operate via a heat absorption mechanism. Most notably, the ilmenite sample, optimized by milling at 600 rpm for 120 minutes, yielded the most significant thermal protection, reducing the interior temperature of the model house by a maximum of 3.0°C when compared to the unmodified PVA control film. These findings conclusively affirm that the control of ball-milling parameters directly governs the resulting particle size, crystalline size, optical behavior, and ultimately the IR-shielding performance of the natural mineral-based coatings. This research validates the potential of nanosized Thai natural minerals as cost-effective and environmentally friendly alternatives to synthetic nanomaterials, establishing them as highly promising sustainable fillers for advanced, energy-saving NIR-shielding coatings.

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